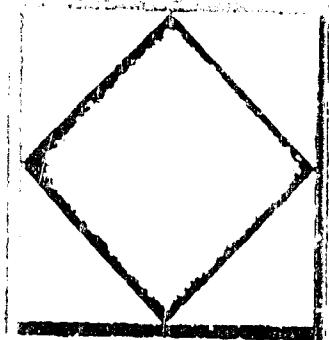


A 330 284



A. M. KINNEY, INC.
CONSULTING ENGINEERS
CINCINNATI, OHIO

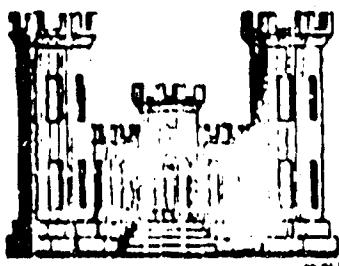
ENERGY ENGINEERING ANALYSIS PROGRAM STUDY

Holston Army Ammunition Plant
Kingsport, Tennessee

EXECUTIVE SUMMARY

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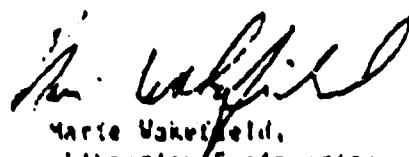
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A handwritten signature in black ink, appearing to read "Marie Wakefield".

Marie Wakefield,
Librarian Engineering

ENERGY ENGINEERING ANALYSIS PROGRAM STUDY
HOLSTON ARMY AMMUNITION PLANT
KINGSPORT, TENNESSEE
CONTRACT NO. DACA CI-SI-C-0670

EXECUTIVE SUMMARY

Prepared by

A. M. KINNEY, INC.
CONSULTING ENGINEERS
CINCINNATI, OHIO

For
MOBILE DISTRICT, CORPS OF ENGINEERS
MOBILE, ALABAMA

January 1983



ENERGY ENGINEERING ANALYSIS PROGRAM STUDY
HOLSTON ARMY AMMUNITION PLANT
KINGSPORT, TENNESSEE
CONTRACT NO. DACA 01-81-C-0072

EXECUTIVE SUMMARY

TABLE OF CONTENTS

<u>Section</u>	<u>Description</u>	<u>Page</u>
1.0	Introduction	1
2.0	Existing Energy Consumption	13
3.0	Energy Conservation Measures	32
4.0	Energy and Cost Savings	33
5.0	Increment A - Energy Conservation Investigations for Buildings	37
6.0	Increment B - Energy Conservation Investigations of Utilities Distribution Systems, SMCs	34
7.0	Increment E (WOD) - Central Boiler Plants	41
8.0	Increment F - Facilities Engineer Energy Conservation Measures (FE-ECM)	43
9.0	Increment G - Non-ECIP Maintenance, Repair and Minor Construction Projects	44

LIST OF FIGURES

<u>Figure No.</u>	<u>Title</u>	<u>Page</u>
1	Area Map	2
2	Energy Consumption (FY-81)	19
3	Purchased Energy Compared to Product Production and Heating Degree Days	20

LIST OF TABLES

<u>Table No.</u>	<u>Title</u>	<u>Pages</u>
1	Building Data Sheets	6-17
2	HAAP Utility Costs	21
3	Present Energy Use for Building Heating	22-27
4	Present Energy Use for Building Cooling	28
5	Present Energy Use for Domestic Water Heating	29-31
6	Recommended Projects and Ratings	34-36

1.0 INTRODUCTION

This volume is a summary of the results of the Energy Engineering Analysis Program (EEAP) study for the Holston Army Ammunition Plant (HAAP).

This EEAP includes energy conservation project recommendations and analyses that will result in a reduction in energy usage. This study also develops data necessary for the Installation-wide Energy Systems Plan.

The study effort is separated into the following increments:

Increment A - Buildings

Increment B - Utilities Distribution Systems and SUCS

Increment C - (Mod) - Central Boiler Plants

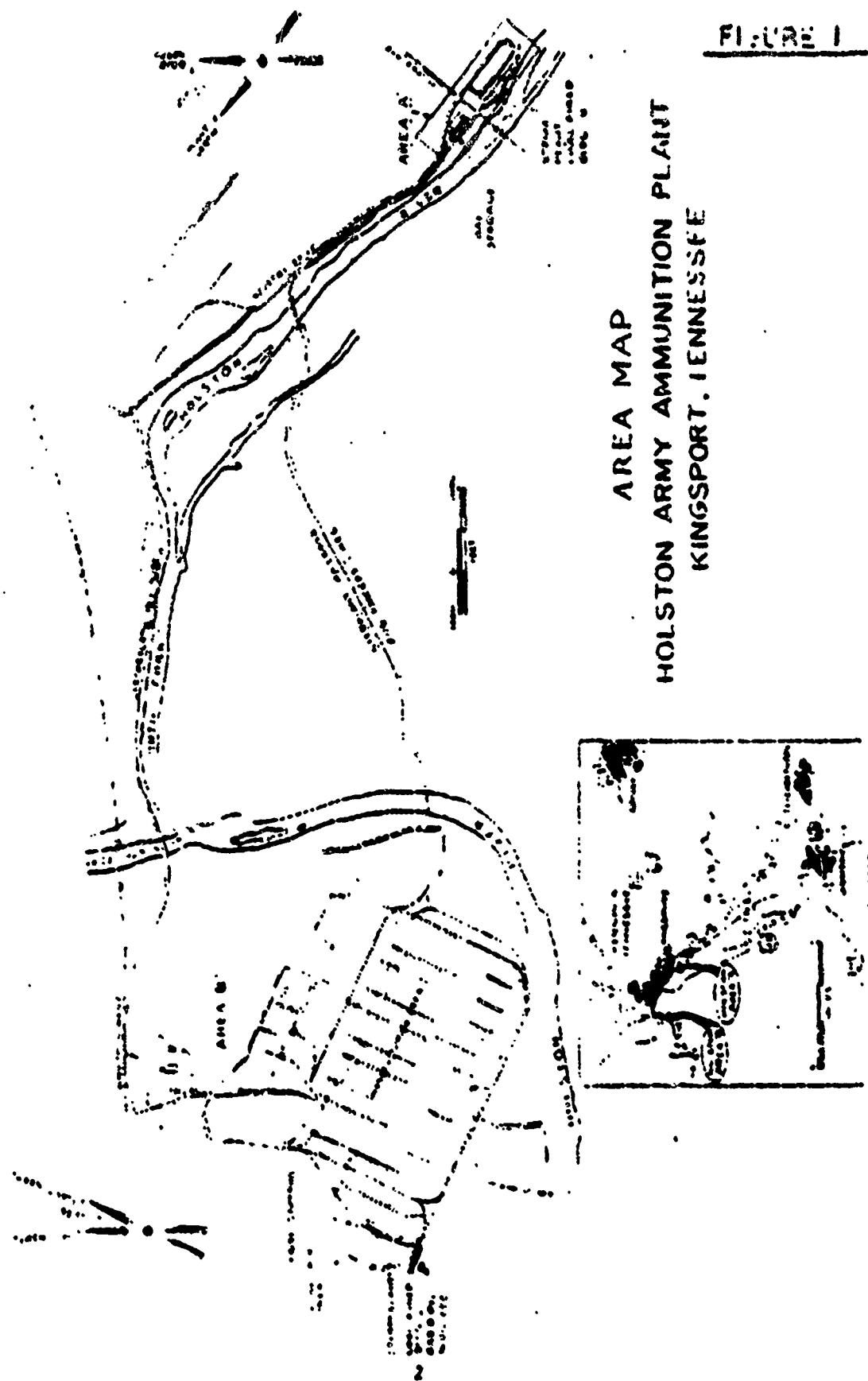
Increment D - Facilities Engineer Energy Conservation Measures

Increment E - Maintenance, Repair and Minor Construction

The HAAP is a Government-owned, contractor-operated (GOCO) military industrial installation under the jurisdiction of the U. S. Army Armament Materiel Readiness Command (ARRCOM), Rock Island, Illinois, built in the early 1920's for the manufacture of explosives as required by the Department of Defense. HAAP is presently operated by Holston Defense Corporation (HDC) at a reduced rate, with the inductive process buildings disconnected from the plant utility systems, but ready to be reactivated quickly in the event full or increased mobilization is required.

Geographically, the plant is divided into two parts known as Area A and Area B, see Figure 1. The total area originally consisted of approximately 6,903 acres (2,938 acres at Area A and 6,215 acres at Area B). Subsequent disposition has reduced

FIGURE 1



Area A to approximately 312 acres, and Area B to approximately 5,913 acres, or a total of 6,225 acres.

Area A is located within the city limits of Kingsport, Tennessee. Area B is located in Hawkins County, Tennessee, 3 miles west of downtown Kingsport, along U. S. route 11-W. The two areas are interconnected by a narrow corridor which contains two acid pipelines, a railroad and a liquid waste line.

Area A is used for the concentration of weak acetic acid into glacial acetic acid and for the production of acetic anhydride. The acetic anhydride is pumped into Area B where explosives are produced. Area B has ten separate explosives production lines with their required supporting facilities. Recovered explosives-free acetic acid is pumped to Area A for reprocessing. Currently, the equivalent of approximately two explosives production lines with necessary support facilities are in operation. The present operating staff of the facility is made up of 1,107 people, including two military and 38 civilian army staff.

As originally constructed, HAP consisted of 553 buildings. However, since the time of completion, the total number of buildings or facilities has been reduced to 333 (not including 101 explosives magazines).

The 333 buildings currently at the plant include 237 buildings which are presently either closed, laid away or otherwise not included in this energy report but which are maintained in readiness for quick activation in the event that increased production rates are required, leaving 126 active buildings with a total floor area of 99,263 square feet. Table I presents the Building Data Sheets, see Pages 6 through 17.

The majority of the active process buildings operate on a 24 hour day, 7 days per week, during which time heat radiated from pipes and process equipment is more than adequate for building heating. The heating systems for these buildings are required only during shutdown periods as freeze protection for water lines and wet type fire protection systems. No significant energy can be saved in these buildings if we exclude process systems.

Original maintenance and office buildings are wood frame construction, no wall insulation, and 6 to 8 inches loose ceiling insulation, with gravity ventilated attic spaces. Some buildings have uninsulated wood floors over ventilated crawl spaces. These buildings are mainly heated by steam cast-iron radiators with manual control. Steam is supplied to most buildings from central steam plants, with the more remote buildings having oil-fired furnaces. Air-conditioning is provided primarily by window type air-conditioning units, except for a few central air-conditioning units using direct expansion coils and air-cooled condensers.

Newer office and service buildings are centrally air-conditioned. Butler type insulated metal buildings or insulated curtain wall construction.

The general level of maintenance at the plant is good and leaves few areas for improvement.

Inspection of the steam distribution system revealed no great break in the insulation, except that steam lines were uninsulated downstream of the isolation valves in the inactive production areas.

The central boiler plants in Area A and B are in very good condition even though they are almost 40 years old. The gas-fired boilers have been operating in

excellent operating condition except for a tube thinning problem at the stoker line of the Area A boilers. Because of their original conservative design, the boilers represent systems equal to or better than present new boiler installations. After a boiler is fired at or near its capacity for a period of a year or more, as would be the case in a full mobilization, the boiler should be inspected by a recognized boiler inspector to determine its capability to handle future full load demands.

HDC, the civilian operating contractor, has done extensive work to reduce energy usage from the base year 1973. Fiscal year 1981 shows a reduction on the order of 40 percent from the base year, as opposed to the federal target range of 20 percent reduction by FY 1985 and 25 percent by FY 2000.

The general level of enthusiasm for energy conservation appears to be quite high, and is maintained at this level by programs sponsored by the operating contractor and the civilian army staff.

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SEARCH DATA SHEET
PAGE 1 OF 12

SEARCH DATA
(1) (2) (3) (4) (5) (6) (7) (8)

SEARCH DATA
(1) (2) (3) (4) (5) (6) (7) (8)

SEARCH DATA SHEETS - PART 1
(1) (2) (3) (4) (5) (6) (7) (8) (9) (10) (11) (12) (13) (14) (15) (16) (17)

FOR CONTINUATION, SEE PART 2, PAGE 2 OF 12

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A. M. Kornegay, Inc.
1000 University Avenue
Seattle, Washington 98101
(206) 467-1242

二

Page 2 - 12

TAMW 1 - MULTIMEDIA DATA SHEETS - PART 2

A. M. ROSENBERG, Inc.
Manufacturers of
Ceramic Glazes
and
Silica Frits

四百一

SEARCH WARRANT
PAGE 2 OF 2

TABLE I - (CONTINUED) *WATER-SOLUBLE BATT& SARTORIS - PART 2*

MUNICIPAL GOVERNMENT

A. M. Hinton, 1921.

A. M. Hausey, Inc.
1000 N. Broad St.
Philadelphia, Penn.
Telephone: 3-0114

AMERICAN DATA SOCIETY
PAGE 2 OF 14

FACILITY - (CONTINUE) DATA SHEET - PART I

TABLE I - CONTINUATION OF THE DATA SHEET - PAGE 7

A. M. Klemmer, Inc.
 1000 University Avenue
 Seattle, Washington 98101
 Telephone 206-467-1000
 Telex 242-2000

MM DEC DATA SHEET
 PAGE 2 OF 12

TABLE 1 - (CONTINUED) MMDEC DATA SHEETS - PART 1
 (in thousands)

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218	2060							0.00	0.00	0.00
219	2061							0.00	0.00	0.00
220	2062							0.00	0.00	0.00
221	2063							0.00	0.00	0.00
222	2064</td									

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TABLE I - (CONTINUED) WILDLIFE DATA FOR 1953 - PART 2

MUNICIPAL GOVERNMENT
PAGE 9 OF 11

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TABLE I - (CONTINUED) BUILDING DATA SWEET'S - PART I

FOR CONTINUATION, SEE PART 2, PAGE 10 OF 12

TABLE 1 - (CONTINUED) ESTIMATED DATA SOURCES - PART 2

SCULPTURE CHINA STREET
PART THE 45

PAGE 1 - (CONTINUED) MTA STATEMENTS - PART I

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TABLE I - (CONTINUED) BUILDING DATA SHEETS - PART 2

2.0 EXISTING ENERGY CONSUMPTION

Figure 2 shows that for FY 1981, coal and electricity account for 99.3 percent of all the energy consumed at HAAP.

Figure 3 plots the coal and electrical consumptions for the base year 1975 through 1981. Also plotted is equivalent RDX production and heating degree days which are used for the adjusted energy consumption plot.

Table 2 lists the fourth quarter 1981 utility costs that were used as the basis for all economic studies in this report.

Table 3 shows the present building energy use for building heating.

Table 4 shows the present energy use for building cooling.

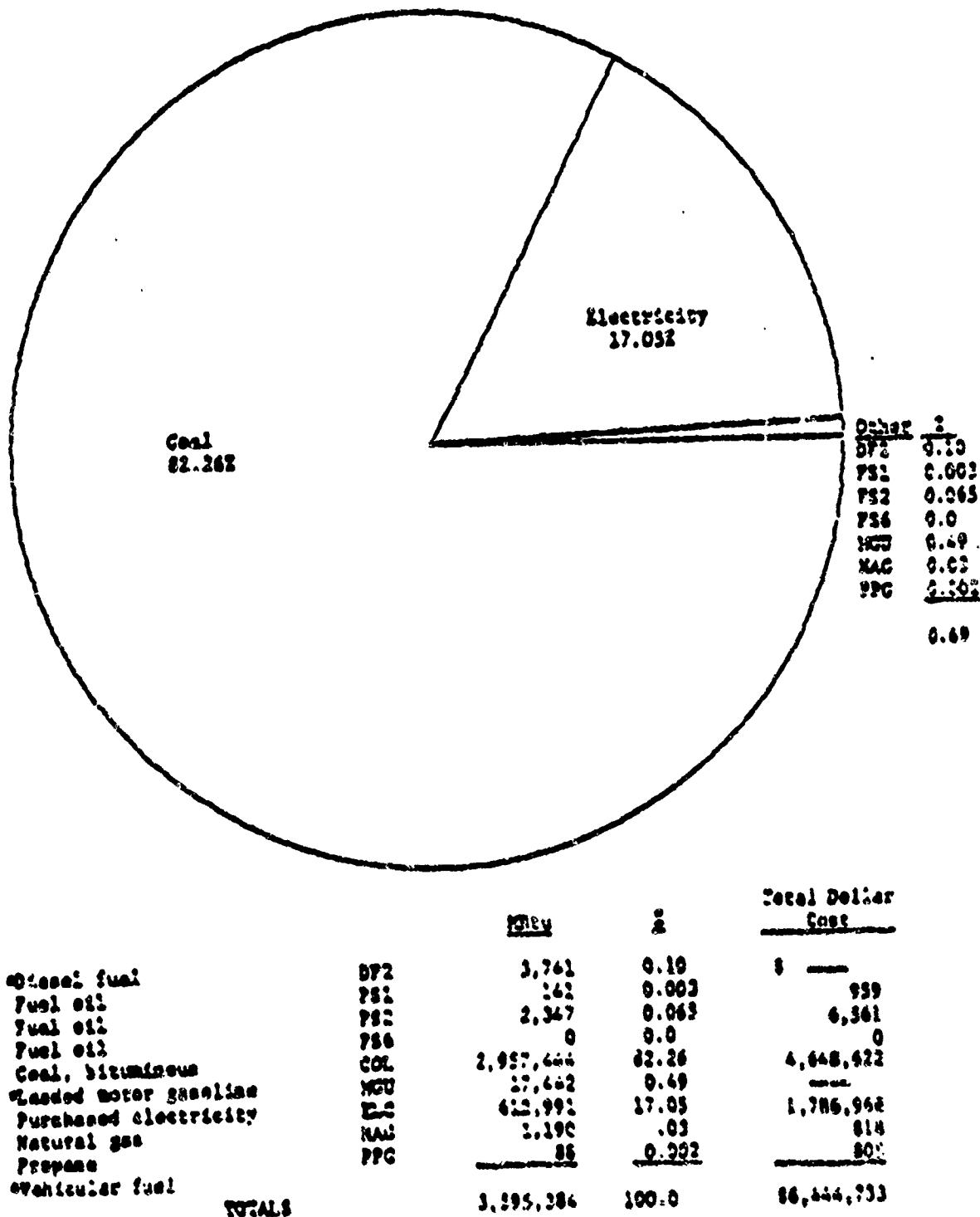
Table 5 shows the present energy use for domestic water heating.

KOLSTON ARMY AMMUNITION PLANT

FIGURE 2

Energy Consumption

FY-81 (Oct. 1980/Sep. 1981)



100 HOUSTON A&P
W.G. HARRIS, KINGSPORT, TENN.
S. 68 921

**A. M. KINNEY, INC.
CONSULTING ENGINEERS
CINCINNATI, OHIO**

File No. 2291 Date 1-16-32
Chas. No. 7410 Date 4-30-2
Conv. No. 848 Date 2-22-32

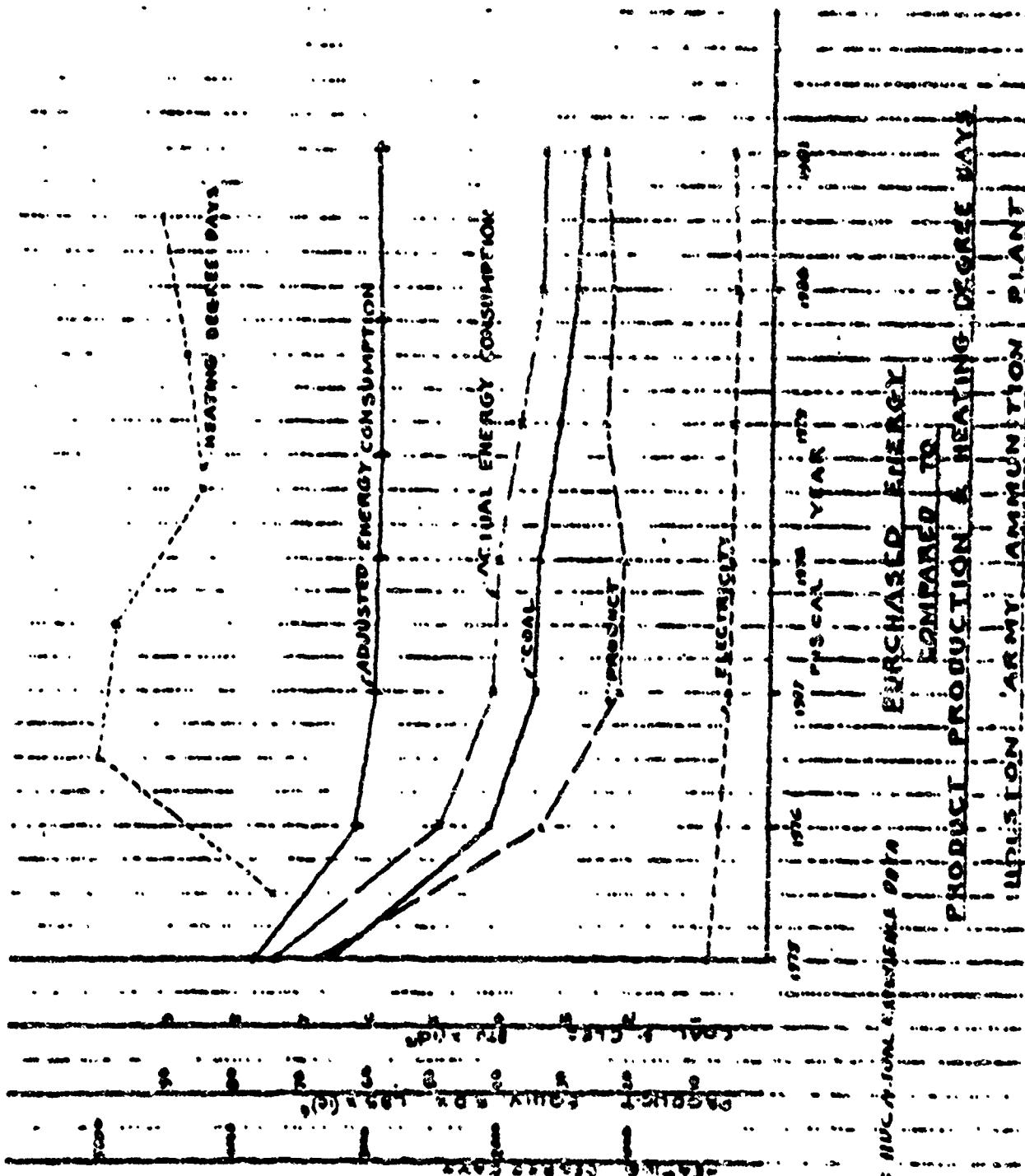


TABLE 2
HAAP UTILITY COSTS

4th Quarter FY 1981

<u>Utility</u>	<u>Units</u>	<u>Area A</u>	<u>Area B</u>
River Water	\$/1,000 gal.	0.0234	0.0231
Filter Water	\$/1,000 gal.	0.1413	0.1093
City Water	\$/1,000 gal.	1.2833	1.3030
Compressed Air	\$/1,000 cu.ft.	0.1963	0.236
Electricity	\$/1,000 kwh	32.10	32.10
Steam	\$/1,000 lb.	2.6746	2.6393

TABLE 3
PRESENT ENERGY USE FOR BUILDING HEATING

Bldg. No.	Design Day Heat Loss (Btu/Hour)	Equiv. Full Load Heating Hours	Annual Energy (Mega Btu)		
			Steam	Electric	Dil
Area A					
1	184,950	2,904	370.9	-	-
9	171,932	649	113.6	-	-
11	22,700	2,004	434.9	-	-
12	63,380	2,004	-	-	135.9
14	312,190	2,004	621.6	-	-
15	2,063,555	2,004	2,131.6	-	-
17	268,623	2,004	533.3	-	-
18	812,433	2,004	121.7	-	-
21	135,260	2,004	271.1	-	-
31	288,300	2,004	577.8	-	-
36	964,730	2,004	191.1	-	-
505	239,200	2,004	519.3	-	-
Area B					
2	461,569	1,625	363.9	-	-
3	530,423	2,334	1,294.7	-	-
6	403,332	2,304	903.7	-	-
7	522,656	2,304	-	-	1,051.2
8	613,649	2,304	1,234.3	-	-

TABLE 3 (CONT'D)
PRESENT ENERGY USE FOR BUILDING HEATING

Site No.	Design Day Heat Loss (Btu/Hour)	Solv. Full Load Heating Hours	Annual Energy (Mega Btu)		
			Solar	Fuel	Oil
<u>Area 3</u>					
8A	129,092	2,394	238.7	-	-
3D	19,474	690	13.4	-	-
9	132,690	690	-	-	91.5
12	143,360	1,320	273.9	-	-
26	1,340,314	1,320	2,193.9	-	-
100	4,194,515	2,000	3,455.8	-	-
101	1,080,409	2,000	2,183.2	-	-
102	2,119,662	2,000	4,247.8	-	-
103	2,320,632	690	1,604.6	-	-
104	840,700	2,000	895.2	-	-
105	335,643	2,000	674.2	-	-
106	823,646	2,000	1,694.6	-	-
108	321,330	2,000	643.9	-	-
110	282,370	2,000	563.9	-	-
116	375,172	2,000	751.8	-	-
118	128,643	690	88.6	-	-
119	54,223	2,000	103.7	-	-
127	132,111	2,000	257.0	-	-
139	117,953	2,000	236.4	-	-

TABLE 3 (CONT'D)
PRESENT ENERGY USE FOR BUILDING HEATING

<u>Bldg. No.</u>	<u>Design Day Heat Loss (Btu/Hour)</u>	<u>Equiv. Full Load Heating Hours</u>	<u>Annual Energy (Mega Btu)</u>		
			<u>Steam</u>	<u>Elect.</u>	<u>Oil</u>
<u>1-33</u>					
136	92,538	2,396	185.4	-	-
150	240,957	690	166.2	-	-
151	664,553	690	312.4	-	-
155 (See T-1b)	303,814	2,394	-	154.7	-
156	507,570	1,822	720.7	-	-
157	62,729	2,394	125.7	-	-
203	657,826	2,394	1,313.3	-	1,313.3
216	75,600	690	52.2	-	-
219	231,453	2,394	474.1	-	-
224	84,026	690	61.6	-	-
231	35,976	690	39.3	-	-
235	736,363	5016.8 ..20	-	122.9	-
313	484,573	2,394	481.1	-	-
321	372,219	1,420	-	-	-
322	331,095	2,394	661.3	-	-
323 (See T-1a)	91,393	2,394	249.3	-	-
324	1,291,930	690	988.5	-	-
325	41,208	2,394	96.4	-	-
326	26,961	1,020	536.8	-	-

TABLE 3 (CONT'D)
PRESENT ENERGY USE FOR BUILDING HEATING

Bldg. No.	Design Day Heat Loss (Btu/Hour)	Equiv. Full Load Heating Hours	Annual Energy (Mega Btu)		
			Gas	Elec.	Oil
Area 3					
536	597,636	1,420	343.7	-	-
535	359,150	2,004	713.7	-	-
634	59,624	1,420	-	84.7	-
4	32,333	693	22.6	-	-
5-1	383,603	693	264.7	-	-
5-3	383,603	693	264.7	-	-
C-3	372,680	2,004	746.9	-	-
C-5	372,680	2,004	746.9	-	-
C-6	297,955	2,004	597.1	-	-
F-3	412,963	2,004	867.3	-	-
F-5	412,963	2,004	867.3	-	-
H-1	199,438	2,004	399.7	-	-
H-3	199,438	2,004	399.7	-	-
H-4	199,438	2,004	399.7	-	-
H-5	199,438	2,004	399.7	-	-
H-6	199,438	2,004	399.7	-	-
J-3	301,483	2,004	604.2	-	-
J-4	301,483	2,004	604.2	-	-
J-6	301,483	2,004	604.2	-	-

TABLE 3 (CONT'D)
PRESENT ENERGY USE FOR BUILDING HEATING

<u>Block No.</u>	<u>Design Day Heat Loss (Btu/Hour)</u>	<u>Equiv. Full Load Heating Hours</u>	<u>Annual Energy (Mega Btu)</u>		
			<u>Sys A</u>	<u>Sys B</u>	<u>Sys C</u>
Area 3					
J-3	301,483	2,004	634.2	-	-
J-4	301,483	2,004	634.2	-	-
J-5	301,483	2,004	634.2	-	-
K-3	130,375	2,004	262.3	-	-
K-5	114,340	2,004	229.1	-	-
L-3	301,483	2,004	634.2	-	-
L-4	301,483	2,004	634.2	-	-
L-5	301,483	2,004	634.2	-	-
M-3	301,483	2,004	634.2	-	-
M-4	301,483	2,004	634.2	-	-
M-5	301,483	2,004	634.2	-	-
N-3	301,483	2,004	634.2	-	-
N-4	301,483	2,004	634.2	-	-
N-5	182,701	2,004	366.1	-	-
V-3	237,280	2,004	513.6	-	-
V-4	182,701	2,004	366.1	-	-
V-5	237,280	2,004	513.6	-	-
W-3	76,383	2,004	152.3	-	-
W-4	76,383	2,004	152.3	-	-
P-3	90.3,340	2,004	1,039.1	-	-

TABLE 3 (CONT'D)
PRESENT ENERGY USE FOR BUILDING HEATING

Bldg. No.	Design Day Heat Loss (Btu/Hour)	Equiv. Full Load Heating Hours	Annual Energy (Mega Btu.)		
			Steam	Elect.	Oil
Area B					
R-3	29,690	2,004	59.3	-	-
%-1	47,846	2,004	95.9	-	-
Office (Bldg. Stor.)	13,619	2,004	-	27.3	-
Motor Control (Aerator)	16,280	690	-	11.1	-
Pump House (Bldg. Waste)	7,718	690	-	5.3	-
Motor Control (Digester)	14,849	690	-	11.6	-
Motor Control (Filter)	11,363	690	-	7.3	-
Bldg. Trans. Pump Bldg.	22,534	690	-	15.6	-
Tank Drain Pump Bldg.	9,412	690	-	6.3	-
Land Fill Office	3,989	2,004	-	20.0	-
Elect. Bldg (Area A-1)	3,216	690	-	5.7	-
Compressor (Area A-1)	3,216	690	-	5.7	-
TOTALS			61,333.1	1,178.4	2,392.1
GRAND TOTAL			<u>65,629.1</u>	<u>1,178.4</u>	<u>2,392.1</u>

TABLE 6
PRESENT ENERGY USE FOR BUILDING COOLING

SIC & No.	Design Day Heat Gain (Btu/Hour)	Annual Energy (Mega Btu)			<u>Total</u>
		<u>Fans</u>	<u>Condenser/</u> <u>Chiller</u>		
<u>Area 3</u>					
12	160,620	215.2	237.4	452.6	
26	366,512	194.7	265.3	460.0	
127	73,756	48.3	63.9	113.7	
134 (Auto Dm)	83,133	17.9	55.2	73.1	
(Admin.)	76,064	39.3	81.7	121.0	
(E&M Equip.)	39,840	33.3	81.4	114.8	
135 (T-1b)	429,341	307.9	461.9	769.8	
136	127,481	91.3	137.0	228.3	
235	369,776	58.5	264.3	322.8	
323 (T-1a)	127,670	20.2	79.1	100.3	
TOTAL				2,765.1	

TABLE 3
PRESENT ENERGY USE FOR DOMESTIC WATER HEATING

Site No.	Water Use (1,000 Gal/Year)	Annual Energy (Mega Btu)	
		Steam	Elect.
<u>Area A</u>			
1	1.6	0.7	•
9	3.3	•	1.3
10	16.4	•	61.4
17	3.3	•	1.3
18	4.7	2.2	•
21	7.0	•	3.2
31	16.4	61.4	•
36	3.1	•	1.4
903	<u>14.0</u>	<u>—</u>	<u>3.5</u>
TOTALS AREA A	53.5	64.3	63.0
<u>Area B</u>			
2	5.9	•	2.7
6	11.3	•	5.3
7	27.3	•	12.3
8	23.7	11.7	•
12	13.6	•	7.1
26	66.3	•	30.4

TABLE 3 (CONT'D)
PRESENT ENERGY USE FOR DOMESTIC WATER HEATING

<u>Bldg. No.</u>	<u>Water Use (1,200 Gal/Year)</u>	<u>Annual Energy (Mega Btu)</u>	
		<u>Steam</u>	<u>Electric</u>
<u>Area B</u>			
190	15.8	-	4.8
192	20.8	-	9.3
193	3.2	-	2.4
196	2,129.5	2,226.3	-
123	1,153.2	832.9	-
115	3.1	1.4	-
116	1.6	-	0.7
119	3.3	-	1.5
127	4.3	-	2.0
135	43.7	-	20.0
136	13.3	-	6.1
139	76.1	-	36.9
136	42.1	-	19.3
137	0.8	-	0.4
263	4.8	-	2.2
219	40.2	-	18.6
315	6.6	-	3.0
322	343.6	130.7	-

TABLE 3 (CONT'D)
PRESENT ENERGY USE FOR DOMESTIC WATER HEATING

Blg. No.	Water Use (1,000 Gal./Year)	Annual Energy (Mega Brn)	
		Steam	Elec.
Area B			
328	6.3	-	3.1
339	1.0	-	0.5
634	1.6	-	0.7
F-3	932.8	363.6	-
F-5	386.3	146.8	-
O-3	13.1	6.0	-
O-5	13.1	6.0	-
P-3	873.4	323.2	-
W-1	<u>3.3</u>	<u>-</u>	<u>1.3</u>
TOTALS	6,343.3	3,636.2	139.2
AREA D			
TOTALS			
Area A	53.3	64.3	62.0
Area B	<u>6,343.3</u>	<u>3,636.2</u>	<u>139.2</u>
TOTALS	<u>6,396.3</u>	<u>3,700.5</u>	<u>137.2</u>
GRAND TOTAL		<u>3,977.3</u>	<u>Mega Brn</u>

3.2 ENERGY CONSERVATION MEASURES

The following areas were investigated for energy conservation:

- g. Architectural. Air infiltration, insulation, storm windows, caulkng, weather stripping, entry vestibules, surplusing buildings.
- h. Heating, Ventilation and Air-conditioning. Outside air dampers, variable air volume, window air-conditioners, recirculation fans, new air-conditioning units, steam heat, heat recovery, burning waste engine oil, cooling tower, radiator valves, air curtain, ductwork, unit heater setback and interlock air-conditioning with lights.
- i. Electrical. Power factor correction, transformer core loss, demand peak limiting, relamping, refixturing and rebalasting.
- j. Plumbing. Shower heads, water heaters, heat recovery, heat pump, solar hot water heater.
- k. Boiler House. Steam venting, combustion airflow, hot water drains.
- l. Utilities. Steam piping insulation, condensate return, coal handling, turbulators, river water pumping, air compressors, biomass fuel, cogeneration, high temperature hot water, wet blowers.

6.0 ENERGY AND COST SAVINGS

Table 6 lists the energy conservation investment program projects and Facilities Engineer Energy Conservation Measures. All projects are to be in operation in FY 1989 unless otherwise noted.

TABLE 6
RECOMMENDED PROJECTS AND RATIOS

<u>Item</u>	<u>Description</u>	<u>Cost (\$.)</u>	<u>E/C Ratio</u>	<u>B/C Ratio</u>	<u>Years to Payback</u>	<u>Savings (Mega Btu)</u>
T-1	Building Energy Conservation Projects	175.8	89.6	3.1	2.1	15,750
T-2	Small Boiler Feedwater Pump - Area A	142.8	382.3	27.0	0.5	56,608
T-3	Small Boiler Feedwater Pump - Area B	175.0	131.1	9.2	1.5	22,285
T-4	Additional Insulation H.P. Steam Pipe - Area B	1,351.0	20.0	1.2	11.0	25,379
FE-ECM-1	Water Flow Restrictors	2.8	505.0	13.7	0.3	1,364
FE-ECM-2	Programmable Clock Controller	3.7	327.6	23.4	0.5	1,151
FE-ECM-3	Refixturing, Reballasting and Relamping Lights					
a.	Replacing Standard Fluorescent Lamps with High Efficiency Fluorescent Lamps - 8,736 Hr/Yr Lamps FY-84	0.729	500	3.44	0.5	365
b.	Refixturing Six Change Houses In Area B, 1983 Project	61.237	127	11.66	1.23	6,982
c.	Replacing Standard Fluorescent Lamps with High Efficiency Fluorescent Lamps - 2,600 Hr/Yr Lamps FY-90	1.257	103	3.55	1.2	127

TABLE 6 (CONT'D)
RECOMMENDED PROJECTS AND RATIOS

<u>Item</u>	<u>Description</u>	<u>Cost (\$1,000)</u>	<u>E/C Ratio</u>	<u>B/C Ratio</u>	<u>Years to Payback</u>	<u>Savings (Mann Biu)</u>
g.	Replacing Standard Ballasts with High Frequency, High Efficiency Ballasts - 2,736 Hr/Yr Operation FY-84	3,930	106	6.0	2.4	618
g.	Replacing Standard Ballasts with High Frequency, High Efficiency Ballasts - 2,736 Hr/Yr Operation FY-88	3,387	32.6	8.23	1.83	280
f.	Refixturing Six Office or Shop Buildings in Area B 1986 Project	62,609	76.4	7.67	1.89	2,338
g.	Replacing Standard Ballasts with High Frequency, High Efficiency Ballasts - 2,736 Hr/Yr Operation FY-91	6,293	69.4	10.0	1.5	436
h.	Refixturing Seven Buildings in Area A, 1986 Project	159,771	66.3	5.87	2.4	6,933
j.	Replacing Standard Ballasts with High Frequency, High Efficiency Ballasts - 2,600 Hr/Yr Operation FY-88	26,191	26.6	2.46	6.2	666

TABLE 6 (CONT'D)
RECOMMENDED PROJECTS AND RATIOS

<u>Item</u>	<u>Description</u>	<u>Cost (\$1,000)</u>	<u>E/C Ratio</u>	<u>B/C Ratio</u>	<u>Years to Payback</u>	<u>Savings (Mega-Btu)</u>
j.	Replacing Standard Ballasts with High Frequency, High Efficiency Ballasts - 2,600 Hr/Yr Operation FY-91	53,061	20.6	2.98	3	1,095
k.	Replacing Existing Street Lighting Fixtures with High Pressure Sodium Fixtures Over a 10 Year Period (1983-1992)	14,519 to 24,529	8.6 to 9.1	2.3 to 2.76	4.8 to 4.3	126 to 126
FE-ECM-4	Feed Pump Recirc. Area A, FY-83	19.9	620	3.29	0.6	11,700
FE-ECM-5	Feed Pump Recirc. Area B, FY-83	19.9	331	4.4	1.1	6,263
FE-ECM-6	Feed Pump Recirc. Area B, Dec. - March FY-89	26.43	69.1	6.9	2.9	1,327
FE-ECM-7	Elect. Driven Deaerator Pump - Area A, FY-83	0	-	-	-	16,663
FE-ECM-8	Elect. Driven Deaerator Pump - Area B, FY-83	0	-	-	-	16,318
FE-ECM-9	Increase Deaerator Pressure - Area B, FY-83	0	-	-	-	7,768

5.5 INCREMENT A - ENERGY CONSERVATION INVESTIGATIONS FOR BUILDINGS

A survey of all buildings was made at the site to determine the condition of the buildings and to locate areas where building energy use could be improved.

This survey resulted in a number of Energy Conservation Measures which were developed into one overall ECIP for Building Energy Conservation Projects (ECIP T-1) consisting of:

a. Install a 12,000 Btu window air-conditioning unit in the shift foremen's office in Building No. 323 and reconnect existing steam heating radiator to existing low pressure steam line. The addition of the small air-conditioning unit to serve the shift foremen will allow the main building air-conditioning system to be shut down during nights and weekends.

b. Install a small air-conditioning unit and air-cooled condensing unit in Building No. 155 and modify existing ductwork, install temperature controls and electrical interlock with existing main air-conditioning unit. The addition of the small air-conditioning unit to serve the reduced number of building occupants during the night and weekend shifts will allow the main unit to be shut down during these periods.

c. Install electronic temperature programmers to automatically set back the thermostat setting of the unit heaters at four buildings in Area A and 19 buildings in Area B. For a list of buildings involved, see ECIP T-1 in Volume IV. The addition of these programmers will allow the unit heaters to operate at a lower temperature during night and weekend unoccupied hours.

g. Install variable frequency motor speed controllers on the supply and return fan motors on the variable air volume air-conditioning system in Building No. 26. The addition of the speed controllers will replace the use of constant speed fan motors with inlet dampers to control the volume of air handled by the system. The inlet vane dampers reduce the required power input to the motor somewhat; however, adding variable frequency controllers substantially reduces the required power input to the motor.

g. Install 3-1/2 inches of insulation to the underside of uninsulated floors that are over unheated crawl spaces in Buildings No. 2, 4 and 6. The addition of this insulation will reduce the building heat loss during the winter heating season.

g. Install an entrance vestibule at an exterior door and limit the use of all other exterior doors as emergency exits only, in the change houses, Buildings No. 1a, 2a, 3a, 103, 135, 176, 219, 322, F-3, F-5 and P-3. The addition of vestibules and restricting the use of the other doors will reduce the amount of air infiltration in the winter, thus reducing the amount of building heat required.

g. Install automatic temperature control valves on steam heating radiators in Building No. 1 in Area 3 and Building No. 3 in Area 3 to thermostatically control the steam supply. The automatic control valves will replace existing manual shutoff valves. The addition of the automatic temperature control valves will allow for accurate space temperature control, preventing overheating, thus saving on the use of steam.

6.0 INCREMENT B - ENERGY CONSERVATION INVESTIGATIONS OF UTILITIES DISTRIBUTION SYSTEMS, EMCS

Increment B is the study of all on-Base utility systems and the consideration of Energy Monitoring Control Systems (EMCS).

The on-Base utility systems are generally in good repair. The systems have been reviewed and improved in the past for energy conservation. The following are the energy conservation recommendations and conclusions resulting from this study:

- a. Install additional insulation to the high pressure steam distribution piping in Area B.
- b. It is not economical to add additional insulation to the high pressure steam distribution piping in Area A or the low pressure steam distribution piping in Area B.
- c. It is not economical to install a condensate return system in Area B.
- d. Continue the steam trap maintenance program.
- e. Install smaller turbine-driven boiler feedwater pumps in both Area A and Area B boiler houses.
- f. Install a boiler blowdown heat exchanger in the flash tank drain after the excess steam venting from the 5 psig steam system is eliminated.
- g. Installation of turbulators in Area A waste heat boilers is not justified at the present low steam load.
- h. Continue to monitor the recently implemented program to not operate the on-road river water pump.

j. Incorporate, in future replacement of air compressors, an air dryer that utilizes the heat of compression.

j. A Base-wide Energy Monitoring and Controls System (EMCS) was investigated, but was found to be not feasible at this plant due to the limited energy savings which would be accomplished, and to the higher than average cost of transmitting the control and reporting signals over the long distances involved.

Local time clock controls are recommended for individual buildings.

7.3 INCREMENT E (Mod) - CENTRAL BOILER PLANTS

Increment E (Mod) is a program of modernization for existing central boiler plants. HAAP is served by similar central boiler plants in Area A and Area B, which are each about 11 years old and located about 6.3 miles apart. See Map, Figure 1, Page 2.

The coal-fired boilers are generally in excellent operating condition. The boilers have been derated due to a lack of fan capacity to handle the added particulate removal equipment. Each steam plant is capable of meeting the approved mobilization plan (Sierra VI), assuming the electrostatic precipitators with the pulverized coal-fired boilers are repaired or replaced as previously planned.

7.1 Existing Plans

It is recommended that the following existing plans be implemented:

4. Modernize the coal handling systems.
5. Continue the program of adding boiler overfire air systems to the stoker-fired boilers.
6. Add an oxygen analyzer to one boiler to help control excess combustion air on a test basis.
7. Replace the above mentioned electrostatic precipitators.

7.2 Results

The following is recommended or concluded as a result of the Increment E (Mod) investigations:

8. Biomass, in the form of wood, could be burned in the Area B stoker-fired boilers. This requires the addition of wood handling equipment to the prepared coal handling system.

- b. Install a cogenerating turbine generator in Building B-6, Area B. Convert the existing high pressure steam header north of the G buildings to a low pressure steam header connecting the turbine generator to new distribution piping to the production buildings presently in operation.
- c. The soot blower controls should be automated.
- d. All boilers not required to be operated should be placed in a true layaway condition.
- e. The boiler combustion air to the forced draft fan should be ducted from outside in the winter and from the upper areas of the boiler house in the summer.
- f. No attempt should be made to burn any fuel other than natural gas or oil in the presently laid-away boilers in Building No. 222.
- g. The existing ash handling systems are adequate even though they do not reflect the latest removal methods normally found in plants of this size.
- h. Installation of a high temperature hot water heating system for modernization purposes is not feasible.

8.0 INCREMENT F - FACILITIES ENGINEER ENERGY CONSERVATION MEASURES (FE-ECM)

Increment F develops recommendations that can be used to update the Installation Base-wide Energy Systems Plan. These recommendations include changes, alterations or modifications to systems operations that are under the control and funding authority of the Facilities Engineer.

The following are the recommendations resulting from this study:

a. Reduce the excess low pressure steam venting to atmosphere from each boiler house by incorporating the following operational modifications:

(1) Operate the motor driven deaerator feedwater pump with the turbine-driven pump on warm standby in both Area A and Area B boiler houses.

(2) Reduce the boiler blowdown flows to the minimum acceptable level.

(3) Increase the Area B deaerator and low pressure steam system pressure.

b. Programmable time clocks with temperature setback are recommended for individual buildings.

c. Water flow restrictors are recommended for the shower heads at all change houses and other areas where shower facilities are provided.

d. Reballasting, relamping and refixturing are recommended for all buildings as replacements are required.

e. Additional training of personnel is not required.

9.0 INCREMENT G - NON-ECIP MAINTENANCE, REPAIR AND MINOR CONSTRUCTION PROJECTS

Increment G is the identification of non-ECIP maintenance, repair and minor construction projects.

The level of maintenance presently performed at HAAP is typical of a well-run chemical plant.

One major maintenance item was found. The multiport relief valve in each boiler house low pressure steam system should be inspected for leakage after it has been determined that high pressure steam is required for makeup to the low pressure system.

It is recommended that an automatic recirculation control system be installed in each boiler feedwater pump recirculation line as a minor construction project in order to reduce the excess low pressure steam venting. Automatic shutoff of the recirculation flow at feedwater flows above the pump minimum flow will reduce the pump horsepower requirements, which will reduce the turbine exhaust low pressure steam flow.